복합 좌우향 전송선로를 이용한 UWB 대역통과 필터의 설계
(Design of UWB Bandpass Filter using CRLH Transmission Line)
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요 약
본 논문에서는 덤벨형 결함 접지면 구조를 갖는 복합 좌-우향(CRLH) 전송선로를 이용하여 초광대역 대역통과 필터를 설계하였다. 결함 접지면 구조와 마이크로스트림 인터디지털 캐패시터를 이용하여 CRLH 전송선로를 구현하고 이것을 이용하여 필터를 설계하였다. CRLH 전송선로는 저역통과와 고역통과 필터의 복합적인 특성을 나타내는데, 그것들의 차단주파수를 잘 조절함으로서 초광대역의 대역통과 필터의 특성을 얻을 수 있다. UWB 필터 특성을 얻기 위해 1, 2, 4, 8 셀을 갖는 CRLH 전송선로에 대해 시뮬레이션하였고, 본 논문에서는 결과를 검증하기 위해 4 셀 구조의 UWB 필터를 설계 제작하였다. 측정된 결과는 시뮬레이션 결과와 일치하며 5GHz 중심주파수에서 88%의 넓은 대역폭을 갖는다.

Abstract
A novel design method of ultra wideband bandpass filter using CRLH transmission line with Dumbell type DGS is presented in this paper. Defected Ground Structure and microstrip interdigital capacitor are used to design the ultra wideband (UWB) filter. CRLH transmission line has composite characteristics of low pass and high pass filter. As control of cutoff frequency of low pass and high pass response on CRLH transmission line, we can get characteristic of UWB filter. We designed and simulated for CRLH transmission lines with one, two, four, and eight cells. A UWB filter using four cells CRLH is designed and fabricated to verify the results. The characteristics of designed filter have center frequency of 5GHz and relative bandwidth of 88%.

Keywords: Composite Right–Left Handed (CRLH) Transmission Line, Defected Ground Structure (DGS), Ultra wideband (UWB) filter

I. Introduction
Ultra Wide Band (UWB) technology has aroused significant interest of researchers since the U.S. Federal Communications Commission (FCC) approved the unlicensed use of UWB (3.1~10.6 GHz) for commercial communication purpose[1]. To date, numerous studies on planar filter technologies have been explored for UWB applications[2~3]. An example of UWB bandpass filter using stub–loaded multi–mode resonator (MMR) is represented in [4]. A widened upper–stopband is realized by incorporating this MMR with two interdigital parallel–coupled feed lines. The insertion loss obtained is less than 0.8dB, and return loss higher than 14.3 dB with a fraction bandwidth of 114 %; however, its selectivity is rather poor. Recently, classic microwave bandpass filter theory has been well established in designing narrow and moderate bandwidth filters. But it is not suitable for designing filters with a large bandwidth. So, a great effort has been made in designing the ultra
wideband (UWB) bandpass filter with novel structures, and many methods are used to design the UWB bandpass filter\cite{5-6}. In this paper, a novel kind of UWB bandpass filter is designed based on the composite right-/left handed (CRLH) transmission line\cite{7}, which has highpass property at lower frequencies and lowpass property at higher frequencies, thus constructs an UWB filter. Dulbell type defected ground structure and interdigital capacitor are introduced to satisfy the necessity of the filter. The proposed structure has good characteristics of low insertion loss, ultra wide passband, and improved selectivity characteristics. It has low insertion loss of 0.5dB, and fractional bandwidth of 98% at 5GHz center frequency. The structures with different cell number are studied, but a four cell CRLH UWB filter is fabricated and measured, which has good agreement between simulation and measurement results.

II. CRLH Transmission Line

Metamaterial is an artificially engineered structure that gains its material properties from its structure as its intrinsic material composition\cite{8,9}. For the purely right-handed (RH) transmission line as shown in Figure 1(a), it consists of series inductance and shunt capacitance and shows a lowpass response. In contrast, for the purely left-handed(LH) transmission line as shown in Figure 1(b), it consists series capacitance and shunt inductance and shows a highpass response. In lossless condition, we can get cutoff frequencies of RHTL and LHTL in equivalent circuit of Figure 1 as following (1) and (2).

$$\omega_{c R} = \frac{1}{\sqrt{L_R C_R}}$$  \hspace{1cm} (1)

$$\omega_{c L} = \frac{1}{\sqrt{L_L C_L}}$$  \hspace{1cm} (2)

The purely LH transmission line cannot be realized in the natural materials because of unavoidable parasitic RH effect; therefore an artificial transmission line named CRLH–TL was developed to approximate LH characteristics.

Figure 2 displays the infinitesimal equivalent circuit model of the CRLH–TL. The transmission line can be realized by cascading N unit cell with period of $\Delta \phi$. The total length of the transmission line is N times $\Delta \phi$. Each unit cell in this periodic structure includes the series inductance ($L_R$), series capacitance ($C_L$), shunt capacitance ($C_R$) and shunt inductance ($L_L$) in this model.

The equivalent circuit of CRLH transmission line, which consist of a pure RHTL cascaded with a pure LHTL is shown in Figure 2. It takes on bandpass property under the balanced condition, where $\omega_{cL}$ and $\omega_{cR}$ are the high-pass cutoff frequency of pure LHTL and the low-pass cutoff frequency of pure RHTL, respectively. The center frequency of the passband is as following (3).

$$\omega_c = \frac{1}{\sqrt{\omega_{cL} \omega_{cR}}} = \frac{1}{4 \sqrt{L_R C_R L_L C_L}}$$ \hspace{1cm} (3)

Given the values $L_R$, $C_R$, $L_L$, $C_L$ of the CRLH structure has a bandpass characteristic when $\omega_{cL} < \omega_{cR}$. For the requirements of UWB filter under the balanced condition, the key problem is to design...
a CRLH transmission line with larger $L_L, C_L$ and smaller $L_R, C_R$. Although the CRLH transmission line based on the equivalent LC circuit is a bandpass filter in nature the design method is completely different from that of conventional filter.

**III. Proposed UWB Filter**

In this paper, the modified CRLH structure is described by the circuit model as shown in Figure 3. The LH shunt inductance and series capacitor, the RH shunt capacitor and series inductance are similar to those of the conventional CRLH structure of Figure 2. An additional cross-coupled capacitance $C_s$ is introduced to create some novel characteristics. In this paper, the series tank is realized with microstrip interdigital capacitor, and the shunt tank is implemented by dumbbell type defected ground structure.

In Figure 3, the interdigital capacitor was designed with the finger width $g=0.6$mm, spacing between adjacent fingers $s=0.2$mm, the finger length $a=10$mm, line width for 50ohm of $w=2.3$mm. The dumbbell type DGS has length of $a=10$mm, width of $b=2.7$mm and gaps of $c=2.3$mm, $d=4$mm. The proposed bandpass filter is simulated by full-wave EM simulator HFSS.

The $S_{21}$ characteristics for proposed CRLH transmission line of Figure 3 are shown in Figure 4. The $S_{21}$ characteristics are compared when spacing between adjacent fingers is $s=0.2$mm and $s=0.4$mm. When the spacing between adjacent fingers ($s$) is 0.2mm as shown in Figure 4, bandwidth of filter is from 2.2GHz to 7.5GHz. The interdigital capacitor has a relatively larger value of series capacitor $C_L$ while DGS in ground plane will decrease the shunt capacitor $C_R$, which may satisfy the ultra wideband condition $\omega_c \ll \omega_R$. The other parameters are carefully selected to meet balanced CRLH requirement, which avoids the bandgap in the wide pass-band range. We used the board for microstrip line with a dielectric constant of $\varepsilon_r=2.3$ and a
thickness of 1mm. The unit cell as well as the periodic structure is studied. Each cell structure is composed of an interdigital capacitor with a defected aperture on ground plane. The interdigital capacitor was designed with the finger width $g=0.6\text{mm}$, spacing between adjacent fingers $s=0.25\text{mm}$, the finger length $a=10\text{mm}$, line width for $50\Omega$ of $w=2.3\text{mm}$, pitch of each cell $p=9.5\text{mm}$, and the number of fingers $N=3$. The dumbell type DGS has length of $a=10\text{mm}$, width of $b=2.7\text{mm}$ and gaps of $c=2.3\text{mm}$, $d=4\text{mm}$. Simulated frequency response of one-cell, two-cell, four-cell, and 8-cell CRLH structures are compared in Figure 5, which shows an obvious UWB bandpass response with a wide passband range 2.8 to 7.2GHz and a low insertion loss of less than 0.5dB. The relative bandwidth is about 88%. The out-of-band suppression of the UWB filter gets better as the cell number increases.

### IV. EXPERIMENT RESULTS

To validate the theory, four cell CRLH structure was fabricated and measured with Agilent Vector Network Analyzer. Figure 6(a) and 7(b) are configurations of top and bottom side of four cells.

![Configuration of top and bottom side of four cells](image_url)
filter, and Figure 7(a) and 7(b) are photos of top and bottom side of four cells CRLH UWB filter, respectively. The comparison of simulation and measurement results are shown in Figure 8.

V. CONCLUSION

The novel design method of UWB bandpass filter using the composite right-/left handed (CRLH) transmission line is represented in this paper. The DGS and interdigital capacitor are used to construct the basic CRLH structure. The proposed structure has good characteristics of low insertion loss and ultra wide passband. It has low insertion loss of 0.5dB, and fractional bandwidth of 88% at 5GHz center frequency. The structures with different cell number are studied, but a four cell CRLH UWB filter is fabricated and measured, which has good agreement between simulation and measurement results.

REFERENCES


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