

An Eight-Element Compact Low-Profile Planar MIMO Antenna Using LC Resonance with High Isolation

DukSoo Kwon¹ · Soo-Ji Lee¹ · Jin-Woo Kim¹ · ByungKuon Ahn¹ · Jong-Won Yu¹ · Wang-Sang Lee^{2,*}

Abstract

An eight-element compact low-profile multi-input multi-output (MIMO) antenna is proposed for wireless local area network (WLAN) mobile applications. The proposed antenna consists of eight inverted-F antennas with an isolation-enhanced structure. By inserting the isolation-enhanced structure between the antenna elements, the slot and capacitor pair generates additional resonant frequency and decreases mutual coupling between the antenna elements. The overall size of the proposed antenna is only $33 \text{ mm} \times 33 \text{ mm}$, which is integrated into an area of just $0.5 \lambda \times 0.5 \lambda$. The proposed antenna meets 5-GHz WLAN standards with an operation bandwidth of 4.86 – 5.27 GHz and achieves an isolation of approximately 30 dB at 5 GHz. The simulated and measured results for the proposed antenna are presented and compared.

Key Words: Isolation Technology, MIMO, Mutual Coupling.

I. INTRODUCTION

In multi-path environments, a high channel capacity is required in order to send more data in the desired direction. A multi-input multi-output (MIMO) antenna exploits multiple antenna elements to achieve a higher channel capacity that is proportionate to the number of antenna elements [1]. The conventional approach for MIMO applications is to arrange the antennas over more than half of the wavelength to avoid correlation [2]; thus, it extends the physical size of the antenna. Moreover, increasing the number of antenna elements in a mobile device affects MIMO performance due to mutual coupling between antennas.

Several MIMO antenna designs have been proposed to minimize the mutual coupling between antenna elements and to simultaneously decrease the antenna size. The basic approach is

to increase the space between antennas, but the space is limited, especially for mobile applications. Decoupling networks [3, 4], the slit pattern [5], the parasitic element [6], and the electromagnetic band gap (EBG) [7, 8] have been analyzed; however, these methods require additional space on an antenna. In this paper, we propose a compact low-profile planar MIMO antenna that unites eight inverted-F antennas with an isolation-enhanced structure. We designed the proposed antenna to achieve high isolation between the antenna elements and we verified the antenna's function by identifying the surface current and radiation patterns.

II. DESIGN OF THE PROPOSED ANTENNA

The antenna shown in Fig. 1 was designed by expanding the isolation-enhanced structure with the slot and capacitor, as

Manuscript received May 28, 2016 ; Revised July 6, 2016 ; Accepted July 6, 2016. (ID No. 20160528-017J)

¹School of Electrical Engineering, Korea Advanced Institute of Science and Technology, Daejeon, Korea.

²Department of Electronic Engineering/Engineering Research Institute (ERI), Gyeongsang National University, Jinju, Korea.

*Corresponding Author: Wang-Sang Lee (e-mail: wsang@gnu.ac.kr)

This is an Open-Access article distributed under the terms of the Creative Commons Attribution Non-Commercial License (<http://creativecommons.org/licenses/by-nc/3.0>) which permits unrestricted non-commercial use, distribution, and reproduction in any medium, provided the original work is properly cited.

© Copyright The Korean Institute of Electromagnetic Engineering and Science. All Rights Reserved.

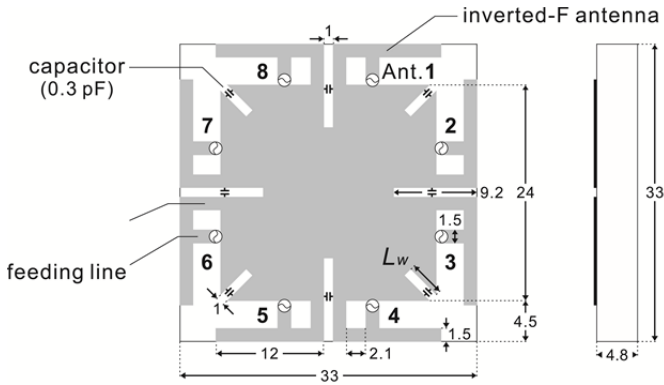


Fig. 1. Geometry and dimensions of the proposed eight-element MIMO antenna (units: mm).

described in [9]. The proposed antenna is fabricated on an FR4 substrate; the size of the antenna is 33 mm \times 33 mm, which is smaller than the conventional $\lambda/2$ MIMO antenna. An inverted-F antenna is flipped and rotated along the ground, forming eight antenna elements. All the antenna elements are arranged by considering an antenna radiation pattern and are the same size, with matching at 5 GHz. Better impedance matching can be achieved by adjusting the length of the upper arm or the distance between the feeding line and the shorting line. All of the antenna patterns with capacitors are inscribed on the top layer. Three FR4 1.6t substrates are stacked to reduce the electrical size per unit antenna element to decrease the size. The isolation-enhanced structure is placed between the two inverted-F antenna elements that are facing each other. Although the distance between two adjacent antenna elements is $\lambda/30$, closer than in [10], the proposed antenna can achieve 30-dB isolation using LC resonance with high isolation.

The 5-GHz surface current of the proposed antenna is depicted in Fig. 2. A slot and capacitor pair is located between two antenna elements. As the slot can be regarded as an inductor, the inductor with a 0.3-pF capacitor causes LC resonance. The resonant frequency of the LC resonance decreases when the slot length located on the four corners (L_w) increases, as in Fig. 3, where $L_w = 4$ mm is chosen as the proposed antenna. If the resonant frequency of the LC resonance matches

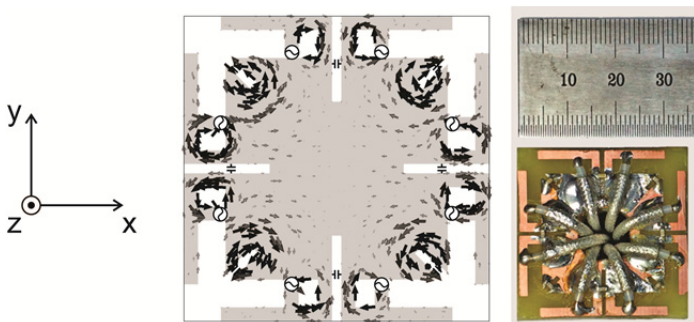


Fig. 2. Surface current distribution and prototype for the proposed antenna.

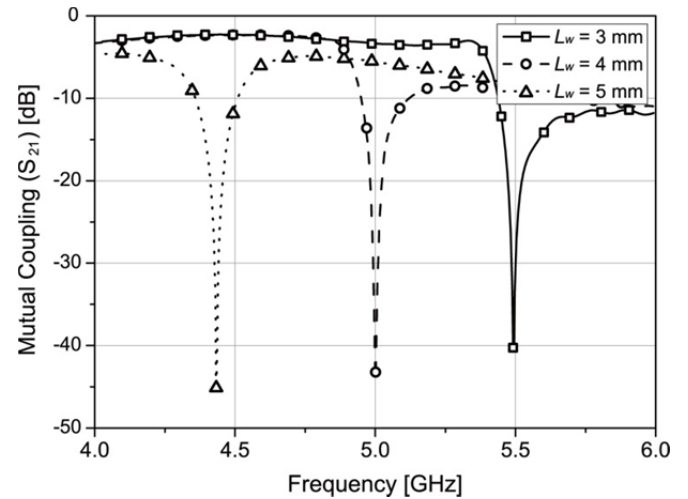


Fig. 3. Comparison of the simulated mutual coupling according to the slot lengths.

with the operating frequency of the inverted-F antenna element, the slot and capacitor separate the ground between the two antenna elements. The surface current along the ground is confined to the LC resonance, which then disturbs the mutual coupling between the two antenna elements. The effect of the isolation-enhanced structure is stronger when the directions of the two antenna elements are crossed. The use of the slot and capacitor ensures high isolation even when the two radiation patterns overlap, e.g. ports 1 and 2, which can result in high coupling between the ports of the antenna.

III. SIMULATED AND MEASURED RESULTS

The return loss and isolation of the proposed antenna are measured with an Agilent 8722ES network analyzer in the measurement range of 4 – 6 GHz. The S -parameter between the antenna elements was obtained from the cable that connects each feeding point of the inverted-F antenna to the connector and the other ports were terminated with 50- Ω termination loads. The simulated and measured reflection coefficients of antenna element 1 are shown in Fig. 4; there was good agreement between the simulated and measured responses. The measured -10 dB impedance bandwidth (S_{11}) is 4.86 – 5.27 GHz, and the reflection coefficients of each antenna element are roughly similar since all the antenna elements are identical. Fig. 5 depicts the simulated and measured isolations from antenna element 1 to the neighboring antenna elements. The measured results reveal that the isolation-enhanced structure in the proposed antenna ensures approximately 30-dB isolation at 5 GHz (f) between antenna elements.

Fig. 6 shows the simulated and measured radiation patterns at 5 GHz for ports 1, 2, 3, and 8 in the proposed antenna. The radiation patterns of the inverted-F antennas that radiate in the electrical field are determined by the direction of the upper arm.

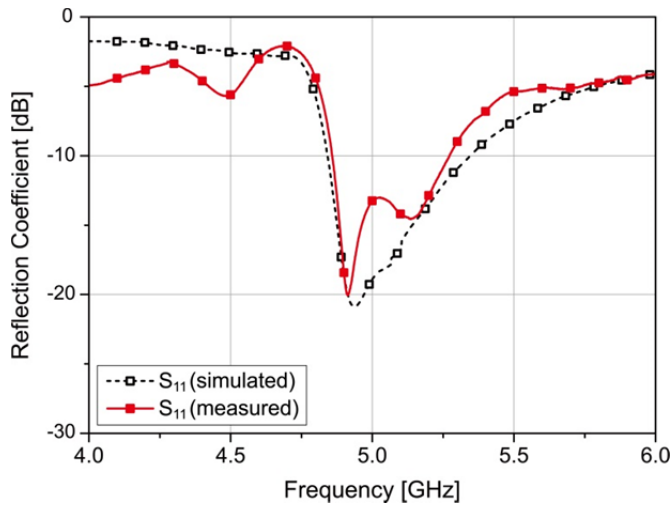


Fig. 4. Simulated and measured reflection coefficients of antenna element 1.

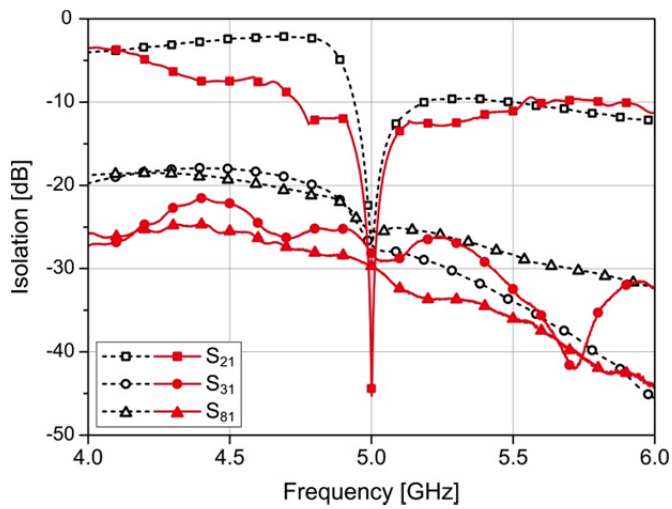


Fig. 5. Simulated and measured isolations between other antennas (ports 2, 3, and 8) and antenna 1 (port 1). The dotted black and solid red lines are the simulated and measured results, respectively.

Table 1. Comparison between compact MIMO antennas

Characteristic	[11]	[12]	Proposed
Bandwidth (GHz)	1.63–2.05	2.4–2.49	4.86–5.27
Measured isolation at f_c (dB)	24	25	30
Electrical size at f_c	$0.43\lambda \times 0.43\lambda$	$0.64\lambda \times 0.48\lambda$	$0.5\lambda \times 0.5\lambda$
No. of elements	4	4	8

The radiation patterns of the antenna elements differ from each other. As can be seen, the radiation patterns of adjacent antenna elements are dissimilar enough to radiate individually with a peak gain of -1.65 dBi. Therefore, it is inferred that the proposed antenna has eight different radiation patterns. Table 1 summarizes the specifications of the multi-port compact MIMO antenna and it also shows the number of integrated

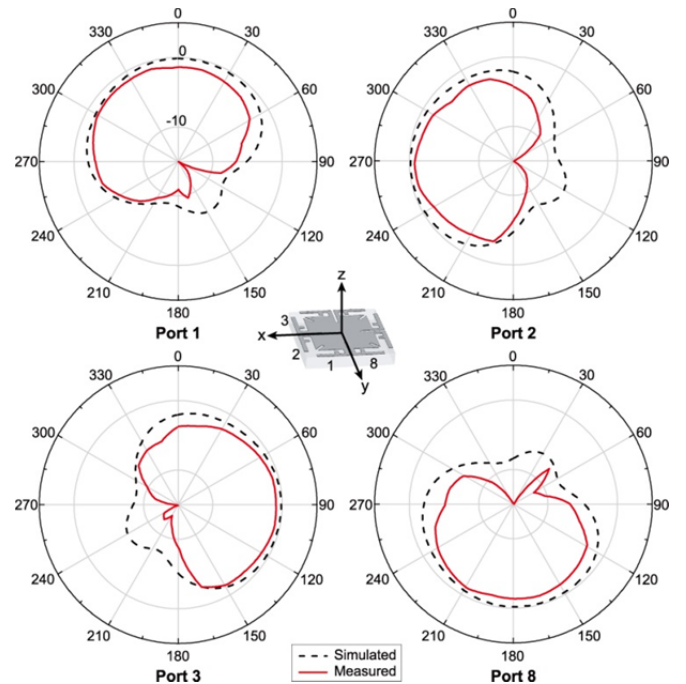


Fig. 6. Simulated and measured radiation patterns in the XY plane at 5 GHz.

antenna elements compared with other previous works. The proposed antenna has attractive features such as approximately 30-dB isolation using LC resonance and wide coverage on the azimuth plane using eight antenna elements.

IV. CONCLUSION

In this paper, we propose a compact low-profile MIMO antenna that integrates multiple antenna elements with an isolation-enhanced structure employing a slot and capacitor for small mobile applications. Our experimental results verify the feasibility of the design incorporating eight antenna elements in a very small area. The proposed antenna is easy to implement within a planar structure and has a high isolation characteristic with a simple slot and capacitor structure. The proposed antenna can be utilized to transfer data with high channel capacity within the operating frequency band.

REFERENCES

- [1] M. S. Sharawi, "Printed multi-band MIMO antenna systems and their performance metrics [wireless corner]," *IEEE Antennas and Propagation Magazine*, vol. 55, no. 5, pp. 218–232, 2013.
- [2] D. M. Pozar and D. H. Schaubert, *Microstrip Antennas: The Analysis and Design of Microstrip Antennas and Arrays*. New York: John Wiley & Sons, 1995.
- [3] S. C. Chen, Y. S. Wang, and S. J. Chung, "A decoupling technique for increasing the port isolation between two

- strongly coupled antennas," *IEEE Transactions on Antennas and Propagation*, vol. 56, no. 12, pp. 3650–3658, 2008.
- [4] M. S. Han and J. Choi, "MIMO antenna using a decoupling network for next generation mobile application," in *Proceedings of the 9th International Symposium on Communications and Information Technology*, Incheon, Korea, 2009, pp. 568–571.
- [5] C. Y. Chiu, C. H. Cheng, R. D. Murch, and C. R. Rowell, "Reduction of mutual coupling between closely-packed antenna elements," *IEEE Transactions on Antennas and Propagation*, vol. 55, no. 6, pp. 1732–1738, 2007.
- [6] K. S. Min, D. J. Kim, and Y. M. Moon, "Improved MIMO antenna by mutual coupling suppression between elements," in *Proceedings of the European Conference on Wireless Technology*, Paris, 2005, pp. 135–138.
- [7] L. Yang, M. Fan, F. Chen, J. She, and Z. Feng, "A novel compact electromagnetic-bandgap (EBG) structure and its applications for microwave circuits," *IEEE Transactions on Microwave Theory and Techniques*, vol. 53, no. 1, pp. 183–190, 2005.
- [8] M. T. Islam and M. S. Alam, "Compact EBG structure for alleviating mutual coupling between patch antenna array elements," *Progress in Electromagnetics Research*, vol. 137, pp. 425–438, 2013.
- [9] J. Park, J. Choi, J. Y. Park, and Y. S. Kim, "Study of a T-shaped slot with a capacitor for high isolation between MIMO antennas," *IEEE Antennas and Wireless Propagation Letters*, vol. 11, pp. 1541–1544, 2012.
- [10] A. C. K. Mak, C. R. Rowell, and R. D. Murch, "Isolation enhancement between two closely packed antennas," *IEEE Transactions on Antennas and Propagation*, vol. 56, no. 11, pp. 3411–3419, 2008.
- [11] S. Zhang, P. Zetterberg, and S. He, "Printed MIMO antenna system of four closely-spaced elements with large bandwidth and high isolation," *Electronics Letters*, vol. 46, no. 15, pp. 1052–1053, 2010.
- [12] H. Li, J. Xiong, Z. Ying, and S. He, "High isolation compact four-port MIMO antenna systems with built-in filters as isolation structure," in *Proceedings of the Fourth European Conference on Antennas and Propagation*, Barcelona, 2010, pp. 1–4.